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# NEW COEFFICIENTS FOR THE SWANSON PPC MODEL AS UTILIZED BY OMEGA AT 10.2 kHz.

A.J. TOLSTOY



Prepared by

## **DEPARTMENT OF TRANSPORTATION**

United States Coast Guard OMEGA Navigation System Operations Detail Navigational Science Branch

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## ABSTRACT

New least squares regression coefficients for the Swanson PPC model at 10.2 kHz have been computed. The data and its deficiencies are discussed. Significant improvement in the accuracy of predictions for station D in the Mediterranean region has been obtained. Indications are that further research into the geomagnetic models is needed.

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## "New Coefficients for the Swanson PPC Model as Utilized by Omega at 10.2 kHz"

### A. I. Tolstoy

#### I. Introduction

The Swanson phase propagation correction (PPC) model is a computational scheme which attempts to semi-empirically model phase variations  $\Delta\phi$  from the nominal as a function of the specific diurnal and geophysical conditions encountered along any given path. The model is comprised of thirteen geophysical submodels which interact in linear combination with each other and which are modified by a solar zenith angle model which accounts for the observed diurnal effects. That is,

$$\Delta \phi_{\mathsf{T}}(\mathsf{P},\mathsf{t}_{\mathsf{o}}) = \sum_{n=1}^{\mathsf{N}} \quad \sum_{i=1}^{13} \ (\mathsf{a}_{i} + \mathsf{b}_{i}\mathsf{f}_{\mathsf{T}}(\mathsf{X}_{n}))\mathsf{H}_{i,n}^{\mathsf{T}}(\mathsf{P}) \; ,$$

where P = point on surface of earth,

to = specific hour of interest,

 $\Delta\phi_{\rm T}({\rm P,t_0})$  = predicted phase variation from nominal of signal from transmitter T to point P at time  $\rm t_0$  ,

ai,bi = linear coefficients for the ith geophysical model,

 $H_{i,n}^{T}$  (P) = geophysical model value at  $n^{th}$  path segment from transmitter T to point P,

X<sub>n</sub> = solar zenith angle at n<sup>th</sup> path segment,

 $f_{\tau}(\cdot)$  = diurnal function which also accounts for abrupt changes at sunrise and

N = total number of path segments (1 path segment is .01 radians in length).

The geophysical models themselves account for geomagnetic field effects, polar cap and auroral zone effects, ground conductivity effects and excitation behavior. For a thorough discussion of these models and their development see references 1-4. It should be emphasized that the Swanson PPC model describes only the behavior of a single, dominant mode signal.

The linear coefficients of the Swanson model are determined by an unweighted least squares regression fit of the model to a data base of observed phase values (1). The coefficients presently in use were determined in 1971 (2), and this paper proposes a new set of coefficients which were generated from a more current data base at 10.2 kHz. In general, the new coefficients are very similar to the old, but it is worth noting that the new coefficients appear to differ greatly from the old coefficients in their fifth through tenth values. These values correspond to the midpath geomagnetic models which were determined by a Fourier fit to theoretical data, and as such their combined rather than their individual effects are what influence prediction. This resultant effect with the new coefficients does not differ greatly from the old resultant effect. However, the new twelfth day coefficient is very different from the old value. This coefficient corresponds to the ground conductivity effects upon excitation behavior. It is not understood why this value is so different from its previous value.

<sup>1.</sup> See reference 5 for further information concerning the application of the least squares estimation technique.

<sup>2.</sup> See appendix A for the coefficient values.

### II. Data Base

The reliability and accuracy of any data base is absolutely critical and cannot be over-emphasized. The most time-consuming portion of this entire study was the intense scrutinizing required before data could be accepted for the final processing. There is, of course, always the danger of over-refining a data base by rejecting valid data which simply may not fit one's scheme of things. Hopefully, this has been avoided by eliminating only that data which was severely erratic or known to be in error. A list of the events (3) which were judgementally deleted is presented in appendix C. In addition, the current data base is comprised of events which meet the following criteria:

\* The events must have occurred after April, 1970 (this eliminates very old signal data which existed prior to active system synchronization with UTC) and also this choice minimized the eleven year solar cycle effect while maximizing the data base;

\* The events must not involve station Forestport, N.Y. (this station has not been operational since Fall, 1972);

\* At least two months of usable data must exist for each fixed monitor site and pair of transmitters (this criterion should eliminate data whose stability is unknown);

\* Events with possible modal interference must be deleted. This criterion is more involved than the others and necessitates dividing the data base into two parts, i.e. a day data base and a night data base. The day data base consists of all events meeting the above criteria minus those events observed within the near field of a transmitting station, i.e. those sites involving LOP x within one megameter of transmitter x. The night data base consists of the day data base minus those events which lie in a predicted night modal interference zone for a given transmitter signal (see reference 6) and

1. have fewer than 5 months of data, or

(Long path interference)

have a sample standard deviation for received phase which is greater than 5 cecs.This criterion resulted in the elimination at night of the following combinations:

Monitor Site	Transmitter
Belem, Brazil	Trinidad
Sabana Seca, Puerto Rico	Trinidad
Orote Pt., Guam	Hawaii
Tsushima, Japan	Hawaii
Spitzbergen, Norway	Norway
Rome, N.Y.	North Dakota
Bermuda	North Dakota
Norfolk, VA.	North Dakota
Makapuu, Hawaii	Trinidad

Finally, the transmitting station monitors all report data involving their near-field transmitter. The path from this transmitter to the site is such a short path that the signal behavior is not accurately described by the models employed herein. For these cases, the data was reprocessed in order to eliminate the offending station. The final data base is described in detail in appendix B. It should be noted that the data base contains no information on transmitters in the southern hemisphere, and only two of the monitor sites (RIO-D and TANAN) lie south of the geomagnetic equator.

An event is defined here to be one month of phase difference data (the difference of the received phases of two transmitters) observed at a given monitor site.

#### III. Results

Overall, for the current data base the new coefficients show significant improvement in the accuracy of their predictions over the old coefficients.

The behavior of each given set of coefficients has been judged by examining the magnitude of the predicted residual errors which they produce. These errors are computed by subtracting a day or night predicted phase difference value from the average day or night phase difference value observed in the data base for a fixed monitor site and LOP pair. The predicted errors will generally be within a few centicycles (cecs) of the errors actually observed. These variations will occur because of the instabilities in the observed data which are caused by random changes in the ionosphere, solar variations, noise (lightning induced), modeling difficulties for paths in solar transition (sunrise and sunset), and receiver errors.

Looking at tables 1-2 we observe that the total root-mean-square (RMS) errors have been reduced from 8.864 cecs (fitting the present data base with the old coefficients which were derived from an old data base) to 5.188 cecs during day hours (4) and from 8.761 so to 5.400 cecs at night. This represents a 42% improvement for day and a 39% improvement for night predictions. Examining the individual pathpair errors we see that only in a few cases do these errors appear to significantly increase in the new fit (5).

These 6 cases are presented in table 3(6). We note that in three of these a poor day (or night) fit is counteracted by an improved night (or day) fit! To be thorough we examined 24 hour plots of the observed data values versus the predicted data values over a typical 30 day period (7). We concluded that in only one case (see figures 1-12) did the complete 24 hour fit deteriorate significantly (8). This one case is SPITS AC where only 4 months of data were used and this data was fairly old (early 1971).

On the other hand, many of the data fits improved dramatically. Specifically, such critical LOP's as Sardinia AD, DG; Farnborough, England AD; and Orote Point, Guam DH showed improvements on the order of 10 cecs (not an RMS value) or more (see figures 12-20). Thus, it becomes apparent that the new coefficients, while not supplying perfect fits everywhere, can reduce many of the gross inaccuracies prevailing in the northern hemisphere with the coefficients currently in use. Moreover, in only one such case did the new coefficients actually produce seriously worse data fits.

It should be again emphasized that the generating data base contained only phase differenced data and only for transmitters in the northern hemisphere. Attempts have been made to evaluate single station predictions for northern, southern and inter-hemispheric paths for the new coefficients, and the results have been quite surprising. In particular, recent single station paths which lie totally within the northern hemisphere are predicted quite well by the new coefficients (see appendix D). Also, available non-computerized data (for August 1976) for the paths from station E to station F and from station F to station E are fit quite well (within 6 cecs) by the new coefficients. However, when examining such inter-hemispheric paths as station A to station E, station D to station F, station G to station

<sup>4.</sup> Day (night) hours are those GMT hours during which both transmitting paths to a monitor site are totally illuminated (in darkness).

<sup>5.</sup> A fit is defined to be significantly worse if a previously good fit (less that 6.5 cecs error) now shows a bias (error is greater than or equal to 6.5 cecs) and the change in error is greater than 3 cecs.

A = Norway; B = Liberia; C = Hawaii; D = North Dakota; E = La Reunion; F = Argentina; G = Trinidad;
 H = Japan. See appendix E for coordinates.

<sup>7.</sup> A "typical" month of data was decided to be one where the day and night phase difference value, were close to the overall mean day and night phase difference values (for that site and LOP).

<sup>8.</sup> A 24 hour fit is defined to be significantly worse if the new RMS error (for 24 hours) is more than 3 cess greater than the old RMS error (for 24 hours).

ICTED ERROR	-3.6	-10.1	1.3		9.0-	9.6	2.6-	a.0-	0.1	5.4	16.7.	-1.7	6.6	1.0	- 4		0.6-	0.1	7.0	9.0-	50.4	-9-1	0.5	-21.3	-20.6	-10.5	19.4	-16.9	8.1	8.2	-11.8	4.0	-0-1	-13.7	-0-3	14.8	-0-2	6.7	-3.2	9.7	2.2	12.7	9.0	-15.0	2.3	-10.4
PREDICTED	28.1	6.64-	22.1	-20.5	-47.2	53.1	0.1-0	-74.0	39.1	61.9	25.5	81.0	56.4	6.5	-30.8	-56.1	-45.2	-43.6	63.4	0.4-	61.4	-8.2	-61.6	-76.6	1-96-1	-37.4	0.00	-80.6	4.8.6	-53.2	4:4	15.0	-96-1	8.5	63.5	1.2	-59.3	66.7	20.8	-35.3	-39.3	34.5	32.2	-98.6	22.8	7.0
TED ERROR	6.0		9.7-		2.3	6.1	3.7	9.0	3.1	5.0	2.5	4.7-	0.3		0.0	4.4	-0.3	9.0	9.0	0.8	5.6	4.7.1	-2.0	-19.2	8.0-	4.4	3.7	-13.7	4.00	6.5	9.2-	-2.6.	-2.5	2.8.5	-3.0	7.3	2.5	-3.5	6.4	1.0	-1.7	2.4	12.2	200	0.1	2.1-
PREDICTED	17.5	-57.8	24. 5	7.45	-50.5	56.1	-10.0	-75.4	36.1	65.8	33.0	87.5	35.3	7.4.7	152.4	-55.7	-53.9	-49.1	-5.4	-11.4	72.7	-16.0	-59.5	-78.7	64.9	-49.5	40.4	-83.8	1.9-	-51.4	-4·7	-19.2	-93.7	6.03	68.2	8.7	.56.5	76.9	12.7	143.0	-39.8	43.0	28.6	8.26-	25.0	3.8
OBSERVED	5.4.5	-56.0	6.65	5.12	-47.8	65.8	-6.3	7.4.7	39.2	4.99	2000	80.1	35.6	7.5	0-14-	-51.3	-54.5	-43.5	-13.9	-10.6	81.8	17.4	-61.5	9-76-	-71.8	-54.0	23.8	-97.5	9.3	-45.0	-7.3	-21.8	-96.5	0.7-	65.2	16.0	10.0	73.4	17.6	-37.9	-41.5	47.2	8.04	198.1	25.1	-3.4
WEIGHT	1.60	1.00	1.00	00.1	1.00	1.00	1.00	1.00	• 0	1.00	000	1.00	1.00	0.0	1.00	1.00	1.00	1.00	000	1.00	1.00	1.00	1.00	0.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.0.	1.00	1.00	1.00	1.00	1.00	1.00	0.	00	• 0	1.00
LOP	AC	46	66	74	90	A6	AC	99	AC.	A G	95	P.C.	AG	99	50	93	A.D	AD	06	A6	AD	90	96	AG	AD	46	AU	A6	90	60	AC	AD	93	90	AG	10	AC CD	AH	AC	A CA	90	60	90	98	04	AG
SITE	BERMU	BERMU	NELC.	HOME.	ROME,	SARDI	WALES	RERMII	CORAL	FARNB	COLLE	SP115	TANAN	RESOL	MONIE	PIARC	MAKAP	ROME,	RERMII	LA-MO	SARDI	SARDI	0-014	RIO-D	NORFO	NORFO	PANAN	BELEM	CA-MO	BELEM	LA-MO	R10-0	H10-0	FARNB	NEA.M	NE BOR	SAHAN	NEA.M	PIARC	CAPAC	SABAN	TSUSH	HESTM	SABAN	VILAN	VILAN

TABLE 1

TABLE OF RESIDUAL ERRORS (DAY)

Market   Color   Wilder	OTHE .	100		- Carried Carr	PREDICTED	FRROR	DDEDICTED	FPROP
CG         100         -5.8         -2.9         -5.3         -0.9           CG         100         -1.4         -2.9 <th>SILE</th> <th></th> <th>WEIGHT</th> <th>OBSERVED</th> <th>The factor of the same of the</th> <th>9-0</th> <th>-5.7</th> <th>0.8</th>	SILE		WEIGHT	OBSERVED	The factor of the same of the	9-0	-5.7	0.8
CG         1.00         -2.8         -2.9         2.8         -1.0           AG         1.00         -2.8         -2.9         2.8         -2.9         -2.9           AG         1.00         -2.5         9         -2.9         -2.9         -10.6           AG         1.00         -2.5         9         -2.9         -2.9         -2.9           AG         1.00         -2.9         -2.9         -2.9         -2.9         -2.9           AG	NELC.		1.00	7.51	0.01	3.5	4 0	2.6-
CG         1.00         -15.4         -2.4         2.4         -10.7           AG         1.00         -22.0         -35.4         2.4         -10.9           AG         1.00         -22.0         -35.4         2.5         -19.9           AG         1.00         -22.0         -35.4         2.5         -19.9           AG         1.00         -22.0         -35.4         2.5         -19.9           AG         1.00         -22.0         -35.4         -25.0         -19.9           AG         1.00         -22.0         -35.4         -25.0         -19.9           AG         1.00         -3.4         -2.5         -25.0         -25.0           AG         1.00         -3.4         -2.5         -2.5         -2.5           AG         1.00         -3.4         -3.5         -2.5         -2.5           AG         1.00         -3.4         -2.	ROME.		1.00	-5.8	-2.5	2000	0.01	3.0
A6 1.00 -15.6 -19.0 C. 4.4 C. 4.5 -19.9 C. 6.4 -19.0 C. 6.4 C. 6.	MIAMI		1.00	1.4	-2.4	2.0	-1	0.0
A6 1.00 -22.0 -24.4 5.5 -23.7 AC 1.00 -22.0 -24.4 5.5 -23.7 AC 1.00 -25.9 -24.3 5.5 -23.7 AC 1.00 -13.8 -23.4 -2.3 -3.3 -11.7 AC 1.00 -3.4 -2.3 -3.3 -3.3 -3.3 -3.3 -3.3 -3.3 -3.3	BERMU		1.00	-16.6	-19.0	4.7	-10.6	0.0-
A6 1.00 -25.9 -15.5 -9.015.7 -9.6 -13.7 -9.6 -13.7 -9.6 -13.7 -9.6 -13.7 -9.6 -13.7 -9.6 -13.7 -9.6 -19.3 -9.9 -19.3 -9.9 -19.3 -9.9 -9.9 -9.9 -9.9 -9.9 -9.9 -9.9 -	ROME .		1.00	-22.0	-24.4	5.5	6.61-	0.3-
AC         1.00         -15.0         -14.7         -0.2         -11.7           AC         1.00         -13.8         -21.3         -19.3         -19.3           CG         1.00         -10.0         -10.0         -10.0         -10.1         -10.3           AC         1.00         -3.4         -2.6         -5.0         -6.0         -6.1         -6.2         -6.2         -6.2         -6.2         -6.	MIAMI		1.00	-25.9	-35.5	9.6	-23.7	202-
AG 1.00 -13.8 -21.9 8.1 -19.3  AG 1.00 -0.1 -1.0 -1.4 -2.3 1.1 -19.3  AG 1.00 -0.1 -1.0 -1.4 -2.5 -0.0 -0.1  AG 1.00 -0.1 -1.0 -1.2 -0.7 -0.1  AG 1.00 -0.2 -1.0 -0.2 -1.0 -0.2  AG 1.00 -0.2 -1.0 -0.2 -1.0 -0.2  AG 1.00 -0.2 -1.0 -0.2 -0.1  AG 1.00 -0.2 -0.2 -0.1  AG 1.00 -0.2 -0.2 -0.2  AG 1.00 -0.2  AG 1.00 -0.2  AG 1.00 -0.2  AG 1.00 -0.2	REBMIL	1	1.00	-15.0	-14.7	-0.5	-11.7	-3.5
CG         1.00         -1.0         -4.3         3.3         1.1           AG         1.00         -5.1         -6.3         -5.0           AG         1.00         -3.4         -6.9         -6.0           CG         1.00         -3.4         -6.9         -6.9         -6.9           AG         1.00         -3.4         -6.9         -6.9         -6.8         -6.0           CG         1.00         -3.4         -6.9         -6.9         -6.9         -6.9         -6.9           AG         1.00         -3.4         -6.9         -6.9         -6.9         -6.9         -6.9           CG         1.00         -4.0         -7.2         -6.3         -6.9         -6.9         -6.9           AG         1.00         -31.3         -25.0         -6.3         -2.5         -2.6         -2.6           AG         1.00         -31.2         -25.0         -6.3         -2.5         -2.6         -2.6           AG         1.00         -31.7         -25.0         -2.9         -2.9         -2.6         -2.6           AG         1.00         -35.3         -25.0         -2.3         -2.5         -2.6 </td <td>HOME .</td> <td></td> <td>1.00</td> <td>-13.8</td> <td>-21.9</td> <td>8.1</td> <td>-19.3</td> <td>2.5</td>	HOME .		1.00	-13.8	-21.9	8.1	-19.3	2.5
AG 1.00 -5.1 -1.4 -5.7 -5.0  AG 1.00 -3.4 -5.7 -5.0  AG 1.00 -3.4 -5.2 -5.8  AG 1.00 -4.0 -5.2 -5.8  AG 1.00 -4.0 -5.3 -10.4 -3.9  AG 1.00 -29.1 -2.3 -10.6 -2.3  AD 1.00 -33.7 -23.2 -2.3  AD 1.00 -33.7 -22.5  AD 1.00 -8.7 -2.3 -2.2  AD 1.00 -8.7 -2.2  AD 1.00 -9.8 -1.2  AD 1.00 -1.3	REDMI		1.00	-1.0	-4.3	3.3	1.1	-5-1
AG 1.00 -3.4 2.6 -5.0 -6.0 CG 1.00 -3.4 -5.5 CG 1.00 -3.4 -5.9 CG 1.00 -3.4 -5.9 CG 1.00 -3.4 -5.9 CG 1.00 -4.4 -5.9 CG 1.00 -4.4 -5.9 CG 1.00 -2.4 -5.9 CG 1.00 -2.4 -5.9 CG 1.00 -2.4 -5.0 CG 1.00 -2.4 -5.0 CG 1.00 -2.4 -5.0 CG 1.00 -2.4 -5.0 CG 1.00 -31.3 -25.6 CG 1.00 -31.3 -25.6 CG 1.00 -31.3 -25.6 CG 1.00 -31.7 -27.6 CG 1.00 -31.7 -31.7 -27.6 CG 1.00 -31.7	CORAL		1.00	-6-1	-1.4	-4.7	-5.0	-1.1
CG         1.00         13.7         15.1         -1.3         8.6           AG         1.00         -2.4         -6.9         -6.9         -6.3 <td>FADNE</td> <td>1</td> <td>1.00</td> <td>-3.4</td> <td>2.6</td> <td>0.9-</td> <td>-0.1</td> <td>-3.3</td>	FADNE	1	1.00	-3.4	2.6	0.9-	-0.1	-3.3
AG 1.00 -4.4 -5.9 -2.5 -2.8 -2.8 -2.8 -2.8 -2.8 -2.8 -2.8 -2.8	DANNE L		00.1	13.7	15.1	-1.3	8.6	5.1
AC 1.00	CARAND		1 000	7.4-	6.9-	2.5	-2.8	-1.6
CG         1.00         -6.2         4.3         -10.4         3.9           AC         0.0         -4.8         -6.2         -2.0         -2.0           AC         1.00         -1.6         -2.3         -10.4         -2.0           AC         1.00         -31.3         -25.0         -2.0         -2.0           AD         1.00         -31.3         -25.0         -2.3         -20.5           AD         1.00         -31.3         -25.0         -2.3         -20.5           AD         1.00         -31.3         -25.0         -2.3         -20.5           AD         1.00         -33.3         -25.0         -2.1         -20.5           AD         1.00         -33.3         -25.0         -2.1         -20.5           AD         1.00         -27.6         -27.9         -21.3         3.5           AD         1.00         -27.6         <	TANKE		00.1	0.00	-3.2	-0.7	-4.3	0.5
AC 1.00 -4.8 5.0 -0.2 -1.3  AC 1.00 -29.1 -25.7 5.3 -10.6 -2.0  AD 1.00 -29.1 -25.7 5.3 -20.5  AO 1.00 -31.7 -25.0 -0.3 -20.5  AO 1.00 -31.7 -25.0 -0.3 -20.5  AO 1.00 -31.7 -27.8 -20.5  AO 1.00 -31.7 -27.8 -20.5  AO 1.00 -31.7 -27.8 -20.5  AO 1.00 -27.6 -29.3 1.2 -21.3  AO 1.00 -27.6 -29.3 1.2 -21.3  AO 1.00 -27.6 -29.3 1.2 -21.5  AO 1.00 -27.6 -29.3 1.2 -2.5  AO 1.00 -27.6 -29.3 1.2 -2.1  AO 1.00 -27.6 -29.3 1.2 -2.2  AO 1.00 -27.6 -29.3 1.2 -2.1  AO 1.00 -27.6 -29.3 1.2	DECOI	1	1.00	-6.5	4.3	-10.4	3.9	-10.1
CG         1.00         -4.0         -2.3         -1.6         -2.0           AG         1.00         -3.3         -2.3         -2.3         -2.3           AG         1.00         -29.8         -34.7         5.6         -23.2           AG         1.00         -31.3         -25.0         -6.3         -23.2           AG         1.00         -38.3         -25.0         -6.3         -23.2           AG         1.00         -38.3         -25.0         -6.3         -23.2           AG         1.00         -38.3         -25.0         -6.3         -20.5           AG         1.00         -31.7         -25.0         -6.3         -21.2           AG         1.00         -31.7         -27.8         -21.3         -21.3           AG         1.00         -27.6         -29.3         1.7         -22.5           AG         1.00         -27.6         -29.3         1.7         -22.5           AG         1.00         -27.6         -29.3         1.7         -22.5           AG         1.00         -27.6         -29.3         1.7         -21.3           AG         1.00         -27.6	DESOF		00.1	4	5.0	-0.5	-1.3	6.1
AG 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	MONTE		1.00	0.4-	-2-3	-1.6	-2.0	0-2-
CD         1.00         9.8         7.5         5.3         22.1           AD         1.00         -38.3         -28.0         -6.3         -20.5           AD         1.00         -38.3         -28.0         -6.3         -20.5           AD         1.00         -38.3         -28.0         -6.3         -20.5           AD         1.00         -38.3         -28.2         -2.1         -23.2           AD         1.00         -38.3         -27.6         -27.8         -21.3         -21.2           AD         1.00         -31.7         -27.8         -27.8         -21.3         -21.3           AD         1.00         -31.7         -27.8         -27.8         -27.8         -27.5           AD         1.00         -27.6         -29.3         14.2         -27.5           AD         1.00         42.1         33.2         -4.0         -27.6	2000			-1.5	9.3	-10.9	2.6	-4.3
Ab 1.00	MESUL	1	1 00	0	7.5	2.3	.2.1	7.8
A6 1.00 -31.3 -25.0 -6.3 -20.6 A6 1.00 -38.3 -39.2 -21.1 B6 1.00 -38.3 -39.2 -21.1 A6 1.00 -31.7 -27.8 -31.9 CG 1.00 -27.6 -27.8 -31.2 CG 1.00 -27.6 -27.8 -31.2 CG 1.00 -27.6 -29.3 1.7 -22.5 AC 0.0 -27.6 -29.3 1.7 -22.5 AD 0.0 -27.6 -29.3 1.7 -22.5 AD 0.0 -27.6 -29.3 1.7 -22.5 AD 0.0 -27.6 -29.3 1.4.2 -29.5 AD 1.00 -27.6 -29.4 -20.1 AD 1.00 -27.6 -29.5 -20.1 AD 1.00 -27.6 -29.6 -20.5 AD 1.00 -27.6 -20.2 -20.1 AD 1.00 -27.6 -20.2 -20.1 AD 1.00 -28.7 -20.2 -20.1 AD 1.00 -20.7 -20.2 -20.1 AD 1.00 -20.2 -20.2 -20.2 AD 1.00 -20.	TIARC		1.00	-29.1	-34.7	5.6	-23.2	-5.9
AU 1.00 35.5 29.3 6.3 20.5 6.0 1.00 38.3 -36.2 1.4 7.6 1.00 31.7 -30.9 1.4 7.6 1.00 1.00 31.7 -27.8 -3.9 -21.3 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6	MANAF	1	1 00	-31.3	-25.0	-6.3	-20.6	-10.7
DG         1.00         -38.3         -36.2         -2.1         -23.2           DG         1.00         31.7         -9.2         -21.2         -7.5           AD         1.00         -31.7         -27.8         -3.9         -21.2         -27.8           AD         1.00         -27.6         -27.6         -27.6         -27.5 <td>CADOL</td> <td></td> <td>1.00</td> <td>35.5</td> <td>29.3</td> <td>6.3</td> <td>20.5</td> <td>15.0</td>	CADOL		1.00	35.5	29.3	6.3	20.5	15.0
AG 1.00 31.7 30.9 6.8 21.2 4.6 7.6 4.0 1.00 31.7 2.9 6.7 5.5 6.7 4.0 1.00 11.7 6.2 5.5 6.7 6.7 6.2 6.7 6.7 6.2 6.7 6.7 6.2 6.7 6.7 6.2 6.7 6.7 6.2 6.7 6.7 6.7 6.2 6.7 6.7 6.7 6.2 6.7 6.7 6.7 6.2 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7	SADOT		1.00	-38.3	-36.2	-2.1	-23.2	-15.0
AD 1.00 31.7 30.9 6.8 21.2  AG 1.00 -31.7 -27.8 -3.9 -21.3  AG 1.00 -9.0 11.7 6.2 5.5 6.7  AC 1.00 -9.0 12.9 12.9 1.07  AC 1.00 -9.0 12.9 1.07  CG 1.00 6.2 2.0 2.0  AD 1.00 4.9 6.2 2.0  AD 1.00 28.7 2.0  AD 1.00 28.7 2.0  AD 1.00 4.9 6.6  AD 1.00 -14.7 -5.4 -0.5  AD 1.00 -14.7 -10.3 -9.4  AD 1.00 -16.4 -10.3 -9.4  AC 1.00 -16.4 -0.5 -0.5  AC 1.00 -16.4 -0.5  AC 1.	0-010		1.00	1.2	-0.2	1.4	7.6	4.0-
AG         1.00         -31.7         -27.8         -3.9         -21.3           AD         1.00         -1.7         6.2         5.5         6.7           CG         1.00         -8.0         -6.2         -3.3         3.5           AC         1.00         -8.0         -6.5         -1.3         3.5           AC         1.00         -27.6         -29.3         1.7         -22.5           AC         1.00         -27.6         -29.3         1.7         -22.5           AC         0.0         35.1         -27.6         -29.3         1.7         -22.5           AC         0.0         35.1         -27.6         -29.3         1.7         -22.5           AC         1.00         6.2         21.0         1.7         -22.5           AG         1.00         42.1         33.2         4.8         1.5           AD         1.00         42.1         32.7         -4.0         21.6           AD         1.00         -14.7         -14.0         -2.5           AG         1.00         -14.7         -15.0         -17.3         -0.7           AG         1.00         -2.4	FARNA		1.00	31.7	30.9	8.0	21.2	10.5
AD 1.00 11.7 6.2 5.5 6.7  CG 1.00 -0.8 4.2 -5.1 1.9  CG 1.00 9.6 -29.3 1.7 -22.5  AD 0.0 35.1 2.9 3 1.7 -22.5  CG 1.00 6.2 2.0 1.07 -8.2  AD 1.00 28.7 32.7 -4.0 21.6  AD 1.00 0.1 -14.7 -15.0 0.5  DG 038.5 -10.2 -10.3 2.8  AD 1.00 -16.4 -10.2 -10.3 2.8  AD 1.00 -16.4 -10.5 -29.8  AD 1.00 -16.4 -10.5 -10.3 2.8	NORFO		1.00	-31.7	-27.8	-3.9	-21.3	-10.4
CG         1.00         -9.8         4.2         -5.1         1.9           AC         1.00         -8.0         -6.6         -1.3         3.5           CD         1.00         -27.6         -29.3         14.2         7.8           AC         0.         35.1         21.0         14.2         7.8           CG         1.00         6.2         7.8         4.8         1.5           CG         1.00         42.1         33.4         4.8         1.5           CG         1.00         42.2         -6.1         -2.2         2.2           CG         1.00         42.2         33.4         4.8         1.5           AG         1.00         42.7         32.7         -4.0         21.6           AH         1.00         4.9         -6.1         14.1         -2.1           AG         1.00         4.9         -6.6         14.1         -6.8           AG         1.00         4.9         -6.6         14.1         -6.8           AG         1.00         -7.9         -7.4         -0.1         -6.8           AG         1.00         -7.4         -7.4         -0.5	BELEM		1.00	11.7	6.2	5.5	6.1	0.0
AC 1.00 -8.0 -6.6 -1.3 3.5   AC 0. 35.1 -27.6 -29.3 1.7 -22.5   AC 0. 35.1 2.10 14.2 7.8   CG 1.00 6.2 7.8 4.8 1.5   CG 1.00 4.2 -6.1 -2.2   AG 1.00 42.1 33.2   AD 1.00 28.7 33.2   AD 1.00 4.9    AD 1.00 -1.0   AD 1.0    AD 1.0   AD 1.0    A	A-MO		1.00	. 0.8	4.2	-5.1	1.9	1-2-
CD         1.00         9.6         12.9         -23.3         -23.5           AC         0.         -27.6         -29.3         14.2         7.8           AD         1.00         6.2         7.8         4.8         1.5           CD         1.00         6.2         7.8         4.8         1.5           CD         1.00         6.2         7.8         4.8         1.5           AD         1.00         4.2         33.4         4.8         1.5           AH         1.00         4.9         5.0         -4.0         21.5           AD         1.00         4.9         6.9         -4.0         21.5           AG         1.00         4.9         6.9         -6.9         6.9           AG         1.00         4.9         6.9         -6.9         6.9           AG         1.00         4.9         6.9         -6.9         6.9           AG         1.00         -5.9         -5.4         -0.5         -2.5           DG         0.         -3.4         -5.4         -0.5         -2.5           DH         0.         -2.4         -2.4         -0.7         -18.0	BELEM		1.00	-8.0	9-9-	-1.3	3.5	-11-
AC 027.6 -29.3 14.7 7.8  AD 0. 0. 55.1 21.0 14.2 7.8  CG 1.00 6.2 7.8 4.8 1.5  CH 1.00 42.1 33.2 4.8 1.5  AD 1.00 44.9 6.6  AD 1.00 0.1 -14.0 6.5  AG 038.5 -15.4 0.3 -9.4  DG 038.5 -10.2 7.9  AC 03.6 12.7 -10.3 -18.0  AC 03.6 12.7 -10.3 -18.3  AC 03.6 12.7 -10.3 -18.3	BELEM		1.00	9.6	12.9	-3.0	3.00	1 -
AD 0.0 35.1 7.8 -1.7 5.9 CG 1.00 8.1 3.4 4.8 1.5 GG 1.00 8.1 3.2 4.8 1.5 GG 1.00 8.1 3.2 4.8 1.5 GG 1.00 42.1 33.2 4.0 24.0 21.6 4.9 5.7 -4.0 21.6 4.9 6.9 4.9 6.6 14.1 -6.8 4.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6	LA-MO		.0	-27.6	-69.3	1.00	6.23-	27.3
CG 1.00 B.2 3.4 4.8 1.55 CD 1.00 B.1 3.4 4.8 1.55 AG 1.00 42.1 33.2 4.0 24.6 AD 1.00 42.1 32.7 -4.0 21.6 AD 1.00 6.1 -0.1 -0.1 -0.1 AD 1.00 15.0 -14.0 14.1 -6.8 AD 1.00 -14.7 -15.0 0.3 -9.4 DG 038.5 -21.2 7.9 -0.7 DH 02.4 12.7 -10.1 2.8 AC 1.00 -16.4 -6.3 10.1 2.8 AC 1.00 39.3 30.5 30.5 14.4	TANAN	1	0.	35.1	2.0	7.1-	0.5	0.3
AG 1.00 -8.2 -6.1 -2.2 -2.2 CH 1.00 42.1 33.2 -6.1 -2.2 CH 1.00 42.1 33.2 CH 1.00 28.7 -4.0 21.6 CH 1.00 4.9 6.6 14.0 -1.7 -0.1 CH 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	RIO-D		1.00	2.0	0.4	4.4	5-1	6.7
AG 1.00 42.1 33.2 6.9 24.6 AD 1.00 28.7 32.7 -4.0 21.6 AD 1.00 1.01 -14.0 14.1 -6.8 AD 1.00 16.0 9.6 -0.5 AG 1.00 -14.7 -15.0 0.3 -9.4 DG 038.5 -10.2 7.9 -0.7 OH 016.4 12.7 -16.3 2.8 AC 0. 39.3 39.3 30.5 8.8	SABAN		1.00	0.0	1.6	-2-1	-2.2	0.9-
AD 1.00 28.7 32.7 -4.0 21.6 AD 1.00 4.9 5.6 14.1 -6.8 AD 1.00 16.0 9.6 6.5 AG 1.00 -14.7 -15.4 -0.5 DG 038.5 -15.7 -17.3 -18.0 DH 03.6 12.7 -16.3 2.8 AC 0. 39.3 39.3 30.5 8.8	NEA.M		1.00	7.0-	30.0	0.00	24.6	17.5
AD 1.00 4.9 6.6 -1.7 -0.1  AD 1.00 0.1 -14.0 6.8  AG 1.00 16.0 -5.4 -0.5  DG 014.7 -15.0 0.3 -9.4  DG 028.5 -10.2 -17.3 -18.0  DH 1.00 -16.4 -12.7 -10.1  AC 016.2 -17.4 8.8	LA-MO		1.00	29.7	32.7	0.4-	21.6	7.1
AD 1.00 0.1 -14.0 14.1 -6.8  AD 1.00 15.0 -5.4 -0.5  AG 1.00 -5.9 -5.4 -0.5  DG 038.5 -21.2 -17.3 -18.0  DH 03.6 12.7 -10.2  DH 1.00 -16.4 -6.3 -10.3  AC 03.6 -10.2 -10.3  AC 0. 39.3 30.5 4.4.4	NEA.		1.00	0.4	0.00	-1.7	-0.1	5.0
AG 1.00 16.0 9.6 6.9  AG 1.00 -5.9 -5.4 -0.5 -2.5  DG 014.7 -15.0 0.3 -9.4  DG 038.5 -21.2 -17.3 -18.0  DH 02.4 -0.7  AC 016.4 -10.2 -10.1 2.8  AC 016.2 -17.4 1.2 -8.3  AH 1.00 39.3 30.5 8.8	NE A . R	1	0001	0 - 1	-14.0	14.1	-6.8	6.0
AG 1.00 -5.9 -5.4 -0.5 -2.5 DG 014.7 -15.0 0.3 -9.4 DG 038.5 -21.2 -17.3 -18.0 DH 02.4 -0.7 GH 03.6 -10.2 -10.3 2.1 DH 1.00 -16.4 -6.3 -10.1 2.8 AC 039.3 30.5 8.8	VILAN		00.1	16.0	9.6	6.9	6.9	2.6
DG 014.7 -15.0 0.3 -9.4  DG 038.5 -21.2 -17.3 -18.0  DH 02.4 12.7 -10.2  CH 016.4 -6.3 -10.1  AC 016.2 -17.4 1.2 -8.3  AH 1.00 39.3 30.5 4.4	VIIAN	1	1.00	-5.9	-5.4	-0.5	-2.5	+-9.4
DG 038.5 -21.2 -17.3 -18.0 DH 02.4 -10.2 7.9 -0.7 GH 03.6 12.7 -16.3 2.1 DH 1.00 -16.4 -6.3 -10.1 2.8 AC 010.2 -17.4 1.2 -8.3 AH 1.00 39.3 30.5 30.5	NA III		. 0	-14.7	-15.0	0.3	4.6-	-5.3
DH 02.4 -10.2 7.9 -0.7 6H 03.6 12.7 -16.3 2.1 C.8 DH 1.00 -16.4 -6.3 -10.1 2.8 AC 015.2 -17.4 8.8 14.4	HESTA		0.	-38.5	-21.2	-17.3	-18.0	-20.5
6H . 03.6 12.7 -16.3 2.1 DH 1.00 -16.4 -6.3 -10.1 2.8 AC 016.2 -17.4 1.2 -8.3 AH 1.00 39.3 30.5 8.8 14.4	MAKAP		0.	-2.4	-10.2	6.7	-0.7	-101
AC 016.4 -6.3 -10.1 C.8 AC 015.2 -17.4 1.2 -8.3 AH 1.00 39.3 30.5 B.8	NE A . M	1	•0 .	-3.6	12.7	-16.3	2.1	17.1
016.2 -17.4 1.2 -8.3 14.4 1.00 39.3 30.5 8.8 14.4	OROTE		1.00	-16.4	-6.3	-10.1	8.8	2.61-
1.00 39.3 30.5 6.8 14.4	SABAN	AC	.0	-16.2	-17.4	1.5	-8.3	5.2.
	VILAN	AH	1.00	39.3	30.5	8.0	14.4	6.42
	-			The state of the s		The same of the Paris of the Pa		-

TABLE 2

TABLE OF RESIDUAL ERRORS (NIGHT)

Table 3-Special Cases (new coefficients vs old coefficients)

			dicted lual error*		licted dual error
site	LOP	new	old	new	old
BERMU	AC	6.9	-3.6	0.9	-3.2
HESTM	CD	9.1	5.7	no nig	ht data
MIAMI	AG**	no day	data	9.8	-2.2
SPITS	AC	-7.4	-1.7	no nig	ht data
ROME	AC	3.6	1.0	8.7	5.5
SABAN	AD	2.4	-8.1	14.1	6.9

<sup>\*</sup> units of centicycles

<sup>\*\*</sup>may be subject to modal interference at night

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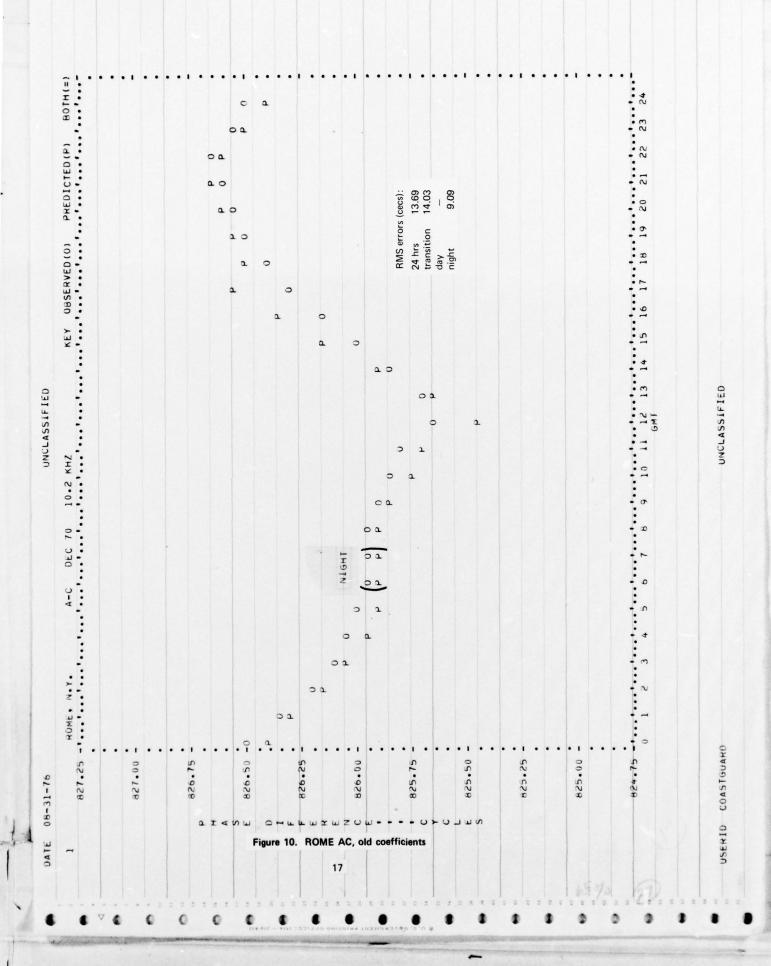
C

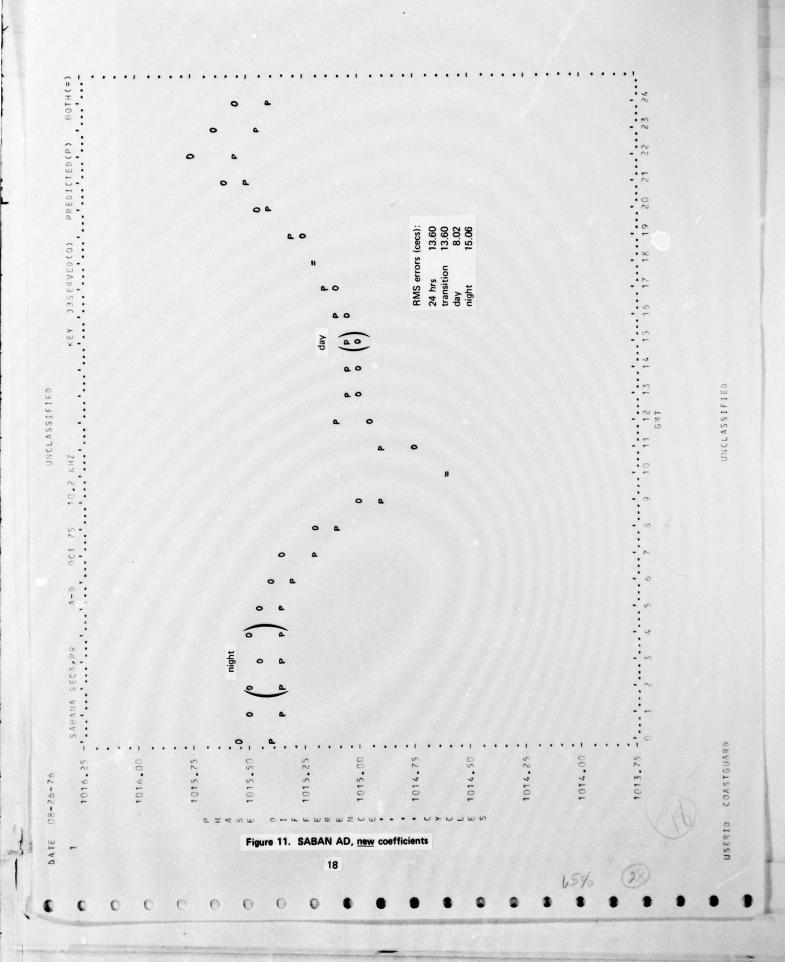
Figure 7. SPITS AC, new coefficients			646.50 - 0 0 0 0 0 0 0 night - night - 646.25 - 646.00 -	645.75 - 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 GMT
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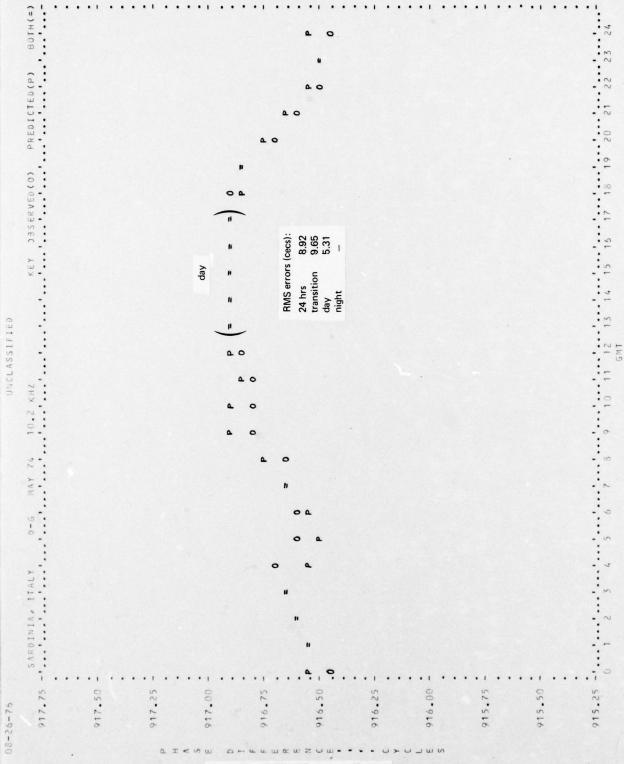


Figure 15. SARDI DG, new coefficients

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F and their reciprocals, some severe errors are encountered for the new coefficients (on the order of 40 cecs)! The data on these paths is quite sparce but considered reliable. Thus, indications are that a serious model deficiency exists for paths crossing the geomagnetic equator. Moreover, the problem is further complicated by the observation that two such inter-hemispheric paths when phase differenced, e.g., A-D at TANAN, do *not* manifest this difficulty. The present data base is totally inadequate to resolve the problem. Obviously the next step in improving prediction accuracy will be first towards expanding the data base to include more southern and interhemispheric single station data and next towards examining further the validity and sophistication of the submodels themselves (particularly the geomagnetic submodels)!

#### IV. Recommendations

At present the only area of the world which suffers from consistent, serious prediction errors is the Mediterranean Sea (represented by FARNB, SARDI and NEA,M data). The Mediterranean errors are well documented in an NELC working paper (see reference 7) and are known to result from inaccuracies (on the order of 10 to 20 cecs) in predicting the signal phase of station D. The new coefficients offer an improvement in predictions in the Mediterranean for all phase differences involving station D with a northern hemispheric transmitter. Thus, it is recommended that the new coefficients be applied in the Mediterranean for all northern hemispheric transmitters. However, these corrections should only be used in a phase difference mode!

The current data base, as demonstrated earlier, is not sufficiently comprehensive in its representation of inter-hemispheric paths nor does it have any information concerning the B, E and F transmitters. In addition, the current software needs modification to realistically process single station phase data. These deficiencies are serious. As such, the generation of any new PPC tables for public use should be restricted to only those areas, i.e., the Mediterranean, which show serious problems now and which we confidently believe can be alleviated by the new coefficients.

#### References

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### APPENDIX A

### New Coefficients (\* 104)

no.	k <sub>D</sub>	confidence interval* (for new coefs)	k <sub>D</sub> (old)	k <sub>N</sub>	confidence interval* (for new coefs)	k <sub>N</sub> (old)
		1 100 100 000137			1	
1	39.41	± 3.4	35.2	9.62	± 4.9	4.4
2	12.91	± 7.5	6.0	11.66	±12.1	9.4
3	0.	-	0.	7.59	±10.5	7.2
4	-8.59	± 9.9	-12.0	18.09	±17.2	14.0
5	-37.66	±23.0	-6.6	-58.4	±42.2	-45.0
6	-29.27	±31.8	0.	-77.78	±47.5	-17.6
7	29.19	±42.0	0.	140.81	±72.9	45.0
8	-16.67	±12.2	1.0	19.16	±26.8	0.0
9	0.	-	0.	-6.36	± 6.4	-4.0
10	0.	-	0.	7.02	±17.6	15.0
11	11.9 **	_	11.9	15.9**	-	15.9
12	56.32	±37.4	10.0	4.48	±49.8	5.0
13	1.53	± 1.8	1.0	0.76	± 2.3	0.9

<sup>\*</sup> determined by student t-distribution.

<sup>\*\*</sup>this coefficient can only be determined by near-field data which could not be processed here. The previous value was retained. Subsequent data analysis has shown this value to be quite accurate.

APPENDIX B

### **Monitor Sites**

CODE	SITE	LAT	LONG
1	NELC, **	32.70800	-117.24650
3	BERMU**	32.26470	-64.87680
9	FARNB**	51.28800	-0.75420
11	SARDI **	39.18100	9.15970
13	ROME, **	43.22400	-75.41020
15	WALES **	65.61220	-168.09170
16	MIAMI **	25.78950	-80.30050
17	CORAL**	64.18670	-83.34220
18	GRAND**	55.17000	-118.84300
19	OSLO, **	59.93830	11.08360
20	SPITS **	78.92330	11.94920
21	RESOL **	74.71388	-94.97333
22	HESTM **	66.52930	12.84530
23	TANAN**	-18.91833	47.55056
24	PIARC **	10.59550	-61.34970
25	MAKAP**	21.30780	-157.65060
26	MONTG**	32.35592	-86.30772
27	LA-MO **	46.55950	-98.63880
28	NORFO**	36.92555	-76.29222
29	RIO-D **	-22.87069	-43.13222
30	TELEC **	39.99567	-105.26225
31	BELEM **	-1.39159	-48.44496
32	NEA,M **	38.10028	23.97833
33	SABAN **	18.45750	-66.21472
34	TSUSH **	34.32470	129.20640
35	OROTE**	13.66890	144.61720
36	VILAN **	38.76138	-27.13116

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10   10   10   10   10   10   10   10	V 61		ARNB	90	885.	2	1.5	0.40	00	• •	•
10	, .		E STE	2 4	707.	+ 15	9.91	0.5	•	-54.1	7.1
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ROME	90	90	0.382	7212	MAKAN	AG	666.6	0.110	7308	BERMU ROME.	90	0.009	1000
		. 0	-	7212	MAKAP			-0.517	1309	BERMU		-0.047	
		. 6	0.350	7212	PIARC		•	0.518	7309	NORFO		0.028	•
NELCO			-0.282	7212	ROME	1		-0.230	7309	ROME.		0.036	
	511116			7301	MAKAP	- 1		-0.613	7310	BERMU	1	+60.0-	1
		, 0-	0.089	7301	ROME.			0.366	7310	NORFO		0.032	-0.164
	1	-	0.389	7301	TANAN			-0.271	7310	8 10-0		-0.453	
-	30.00		666.6	1302	BERMU	-		0.137	7310	810-0	1	-0.150	I
		ĭ	0.356	7302	BERMU		•	0.215	7310	ROME .		0.038	•
	1/4/50	Ī	0.060	7302	BEHMU	1		640.0	1167	MODE		60.03	
		7	0.416	7302	PIARC			0.306	7311	NORTO PER PER		0.029	-
1	YES.		666.6	7302	ROME.		0.018	-0.275	7311	ROME.		0.041	-0.246
1	- 3			7302	TANA	- 6		-0.135	7312	BERMU		666.6	T
		7	0.704	7303	BERMU		0	0.140	7312	BERMU		-0.064	-
	5800		•	7303	BERMU	1			7312	NORFO		-0-005	ī
			, 0	7303	DENMO			•	7312	RIO-0			1
				7303	ROME.		0.029		7312	ROME.			_
	- 1		•	7303	ROME	10	0.031	0	7312	ROME			1
			666.6	7303	ROME .		-0.011	0	7312	ROME,			-0.252
			014.0	7303	SARDI	1	0000	9	7312	SAROI			1
			0.000	7303	SARDI	4	-0.086		7312	SARDI			-
BERNU			666.6	7303	TANAL		666.6	-0-	7401	BERMU			0
	- 2.		199.0	7304	BERMU	100	-0.529	6	1001	BERMU			7
		-0.017	666-6	7304	BERMU		-0.280	•	7401	BERMU			
7205 MONTG	11 12 12 12		-0-310	7304	ROME.		0.020	9	7401	FARNB		666.6	•
				7304	SARDI		-0.059	•	7401	LA-MO		666.6	0
	N AG		666.6	7305	BERMU		-0.207	0	7401	NORFO		666.6	0.256
1	100			7305	DECKAR		012.0		7401	NORFO		-0-057	7
		7 9	0.672	7305	OM-4		0.212	0	7401	910-0		-0.122	9
		, ,		7305	NORFO		0.032	0-	1401	SARDI		666.6	-0
1	23/2	1	100.00	1305	ROME		0.057	6	7401	SARDI	1	666.6	7
			-0.372	7305	ROME.		0.092	0 9	7401	SARUI		666.6	-
	1 - 52		666.6	7305	SARDI	100	0.220	0	7402	BERMU		-0.330	0.150
1		0		7305	SARDI	3.45	0.243	6	7402	BERMU		-0.055	•
		0	6	7305	SARDI		0.021	6	7402	FARNB		666.6	0
-1		-	6	7305	TANAL	1	0.154	6	7402	PARNE	1	0011	7
		î.		7306	BERMU		-0.210	9	2047	NOBEO		666.6	7
1	95	0.045	1	7306	BERMU		0.005	0	7402	NORFO		-0.244	
		-		7306	NORFO	1			7402	NORFO		-0.030	-
		-	6	7306	ROME.		•		7402	SARDI		666.6	1 1
7207 AOM	100		-0-292	7306	ROME.	Bea.	0.070		7402	SARDI		-0.055	?
	- 1		0	1306	SARDI				7402	TANAL	3	0.133	1
			0	7306	SARDI		•		7403	BERMU		-0.063	0
1		-	6	7306	SAROI	9			7403	BERMU		-0.359	
			•	7306	TANAN		0.134		7403	FARNE		0.207	1
	1		0	7307	BERMU				7403	LA-MO		0.124	-
1		•	0	7307	BERMU		0000		7403	NORFO		-0.513	•
		•	0-	7307	LA-MO		0.180		7403	NORFO		-0.121	0
1		•	-	7307	MORFO	1	9.00		7403	MORFO	1	0.018	1
1 FARNB		AG 0.193	-0.458	7307	PIO-D		-0.136	52	7403	SARDI		9.000	? ?
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0.062 9.9999 9.9999 9.9999 0.586 9.999 9.999 9.999 9.999 9.169 9.999 1167 RIO-D RIO-D SARDI SARDI SARDI TANAN TELEC BELEM BELEM BERMU BERMU BERMU FARNB FARNB HESTM SAROT SAROT SAROT TANAD TANAD BEELEM BEERM FARNO FARNO MAKAP MAKAP RRIO-D RRIO-D SARDI SARDI TANAN TANAN BELEC BERMU BERM SARDI SARDI SARDI TANAN 0.200 0.777 0.01 9.999 0.241 SARDI SARDI TANAN TANAN BELEN BERNU PELEN BELEN BELEM BERMU BERMU BERMU FARNB FARNB FARNB FARNB FARNB FARNB SARDI SARDI SARDI SARDI SARDI BELEM BELEM BELEM BERMU BERMU BERMU SSABARA SSABARA SSABARA SSELEN SSELEN SSELEN SSERM SSABARA SARDI 0.146 0.193 0.193 0.186 0.120 0.120 0.113 0.203 0.203 0.204 0.206 0.012 0.076 0.104 0.126 VORFO A-MO SARDI SARDI TANAN BERMU FLEC BERMU BERMU BERMU FARNB FARNB CA-MO NORFO FARNB ARDI SARDI THE STATE 2424 ELEN SARDI 74 60 5 74 74 60 5 74 74 60 6 74 74 60 6 74 74 60 6 74 74 60 6 74 74 60 7 74 74 60 7 74 74 60 7 74 74 60 7 74 74 60 7 74 74 60 8 74 74 60 A# 6

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7505	HESTM	93	162.0-	666.6	1501	SABAN	AU	-0.192	666.6	7511	FARNB	46		-0.484
		,												220
7505	LA-MO	E.	0	666.6	7507	SABAN	00	-0.147		7511	HESTM	90	66.	-0.369
1505	MAKAP	AD		666.6	7507	SABAN	90	-0.085	3	1511	LA-MU	Ac	•	60.00
2051	MAKAP	AG	-0.063	666.6	1507	SARDI	90	0.051		115)	LA-MU	200	100.0	
5054	THERE	90	1+0-0		7507	TELEC	93	660.0-	6000	7611	DE AND		0000	-0.416
1505	NEA.M	A6	0.175		7507	ISUSH	3 4	0.110		7611	NOK OF	100	00	-0.075
1205	NEASM	10	0.010	•	1200	955		107		7511	NF A - M	AD	00	-0.338
COCI	0-01H	A C	6500	•	1500	961 64	2	0.0.0		7511	NEA.M	AG	.14	-0.488
COC	d-oly	33	502.0-	•	7500	DECEM	2 <	-0.016		7511	NEA.M	AH	66666	-0.620
505	10-01×	90	666.6		1500	SEAMO	24	100.0		7611	OROTE	- 63	6666	-0.143
COCL	SABAN	AC	000	•	7500	DEPART	80	-0-150	666.6	7511	PIARC	00	-0.075	0.460
5001	SABAN	3	091.0-	1 0	3500	DEDMI	96	-0.057	0	7511	RIO-0	93	12.0	0.861
505	TOURS	2 9	27	•	7508	FARNA	AD	0.191	666.6	7511	RIO-D	90	-0.085	0.575
2007	SARDI	2 4	0.200	00	7508	FARNA	46	0.210		7511	SABAN	AD	66.6	11.
7505	TANAN	86	0.115		7508	HESTM	90		666.6	7511	SABAN	03	-0.106	0.465
1505	20138	2	0.05	6.47	7508	MESTA	90	.48	666.6	1511	SABAN	90	0	0.316
7506	SEL EM	204	-0-142	00000	7508	OMIN	AC	0.137	666.6	7511	VILAN	AD	66	-0-111
15.06	961 64	2	101-0-	00000	7408	OM-A	AG	0.183	6.	7511	VILAN	AG	0	-0.120
7506	RELEM	200	-0.008		7508	LA-MO	90	0.033	0.059	7512	BELEM	AC	666.6	-0.504
7506	BERMU	AC	-0.047	66666	7508	LA-MO	HS	9.00		7512	HELEM	AD		261.0
1506	BERMU	A.G	-0.164		7508	MAKAP	AO	-0.227		7512	BELEM	25	0.040	199.0
7506	FARNB	-	0.178		7508	MAKAP	90	0.015		7157	TAKNE	2	666.6	017.0-
9051	FARNB	AG	0.231		. 7508	PIARC	AC	-0.056	666.6	2151	LAKNO	Ac	666.6	0.435
1506	HESTH	69	-0.305		7508	PIARC	AO			210	NC A OM	24	•	0 670
9051	LA-MO	AC	0.179	66666	1508	PIARC	00	-0.114	•	215/	NEA.M	2 1		-0-413
1506	LA-MO	94	P		1508	A-OIA	93			2161	NE ROLL	110	•	010.01
9051	LA-MO	90	0.020	0.022	7508	RI0-0	90	960.0-		716/	NEASH	L 5	666.6	413.0-
7586		#3	0.033		1508	SABAN	AC	2	•	3101	24040		•	280
9051	MAKAP	P P	-0.155		7508	SABAN	A C	٠.		7512	CADAN	2 4		0000
1506	MAKAP	¥6	-0.075		1508	SABAN	3	C+1.0-	•	7512	NAGAS	20	420-01	0.530
1506	MAKAP	90	0.082		7508	SABAN	200	-0.00	0 000	7512	24043	90		0.268
1500	NEADM	AG.	161.0	666.6	2000	SAKUI	9 9	0000	0.451	7512	VILAN	40		-0.114
1506	NEASH	E 4	**!*0	9.999	1500	15.50	90		-0.328	7512	VILAN	94	5	7
7506	PIABC	40	-0-166	38.	7508	TSUSH	93	.14	666.6	7512	VILAN	АН		-0.553
7506	PIABC	0	U	281	7509	BERMU	AG	-0.218	0.224	7601	FARNB	AD		-0.550
7506	810-D	AD	-0.195	666.6	7509	FARNB	AG	0.197	-0.489	1601	FARNB	AG		-0.446
7506	810-D	93	-0.215			NEASH	AG	0.143	-0.628	7601	OROTE	10	66.	6.629
7506	RI0-0	90	-0.058		1509	NEA . M	AH	0.063	666.6	7601	SABAN	AD	•	0.274
7506	SABAN	AC	620.0-		1509	-	93	1+2.0-	•	1601	SABAS	3	9	646.0
7506	SABAN	AO	-0.229		1509	SABAN	AG	-0.376	0.570	7601	VILAN	AD	666.6	660.0-
1506	SABAN	69	-0.170	0.535	1509	SABAN		-0.212	•	1091	ATT A	9		61113
7506	SABAN	90	-0.062		7510	BELEM	AD	-0.151	•	7601	VILAN	AH		40.0-
7506	SARDI	94	4		7510	BELEM		0.037	0	7602	FARNB	AD	66.	-0.61
1506	SARDI	90	0.054	666.6	7510	FARNB		666.6	-0-	7602	NEA,M	A		-0.684
2506	TELEC	69	-0.092		7510	FARNO	1	0.189	+	1602	1	-	166.6	1
7507	BELEM	AC			7510	LA-MO		0.227	-0.066	7602	VILAN	AD	666.6	-0.081
7507	BELEM	AB	-9.066	666.6	7510	LA-MO		190.0	0.081	1603	Z X	AD	666.6	
7507	BELEM	00		0.688	1510	LA-MO		666.6	•					
1507	BERMU	90	-0.043		7510	NEASH		666.6	-0.44]					
7507	FARNB	AD			7510	NEA.M		0.173	-0.570				The second secon	
7507	FARNB	46			7510	NEASE	T	666.6	-0.0	-				
7507	HESTM	93		666.6	7510	PIARC	93	-0.082	0.4					
1507	LA-MO	AC	0.181	666.6	7510	810-0	1	-0-172						
7507	LA-MO	AG	0.217	66666	7510	RIO-D	1	-0.093	0					
7507	- KA-MO	93		0.035	1510	SABAN		-0.317	9					
7507	LA-MO	H	0.075	666.6	7510	SABAN		-0.127	•					
7507	MAKAP	AP	-0.104	666.6	7510	SABAN	T	-0.075	1	-				
7507	MAKAP	90	0.011	-0.567	7510	TANAL	AG.	0.021	0.046					
1507	PIARC	AC	400.0	666.6	7510	VILAN		10.0	061.0-					
7507	PIARC.	AO	0.12	666.6	7510	VILAN		0.	-0-111					
1501	PIARC	60	-0-113	0.587	7510	VILAN	90							
			я											
7507	810-0	90	0	0.931	1161	BELEM		666.6						

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# APPENDIX C Judgmental Deletions

CODES: (1) many outages (2) large % error

site	LOP	dates	remarks
BERMU	AC	8/72	flat data
	AG	2,3/72	flat data (no diurnal)
		11,12/73; 1/73	2 + paucity of data
	CG	2,3/72; 1,2/73	1 + 2
	DG	3/74	
HESTM	CD	12/72	2
LA-MO	AG	8/73	1
MIAMI	CG	7/71	1
NORFO	AG	3/75	1 + 2
RIO-D	AD	12/73; 1,12/74	2 + station A through
	AG	12/73; 1/74	modal degeneracy zone at night
ROME	AD	11/72	2 + many PCA's
TANAN	AG	1,4,5/71; 7/72	1 + 2
TELEC	CG	1-8/75	1 + 2
TSUSH	АН	10/75	1 + 2

APPENDIX D
Single Station Paths, Predicted Residual Errors

		new co	efficients	old co	efficients
site	LOP	day	night	day	night
HESTM	С	-3.2	-20.41	8.7	3.2
	D	2.4	14.2	10.9	27.6
	G	7.0	-0.3	11.9	10.6
	Н	-	14.0	-	27.2
MAKAP	A	-1.0	14.12	-12.0	-7.7
	D	-2.4	-7.4	0.0	2.4
	Н	-2.2	1.7	-2.9	2.0
PIARC	A	-5.0	6.9	-12.9	-5.2
	С	-1.3	4.5	-1.2	2.3
	D	-5.5	2.0	5.7	-5.9
LA-MO	A	-1.1	-6.6	-10.2	-10.7
	С	0.5	4.4	0.5	-4.1
	G	2.8	-7.2	4.5	2.5
	Н	-5.3	6.4	7.2	22.5
TSUSH	A	-10.8	-9.8	-11.1	-21.4
	C	9.5	-	2.9	-
	D	5.9	1.7	-9.3	-16.1

<sup>1.</sup> night path only in month of Dec. (data for 1970, 71, 72, 74)

<sup>2.</sup> night path only in month of Dec. (data for 1972, 74)

# APPENDIX E Transmitter Coordinates\*

station	latitude	longitude
A	66° 25′ 15.00″ N	13° 09′ 10.00″ E
В	6° 18′ 19.39″ N	10° 39′ 44.21″ W
С	21° 24′ 20.67″ N	157° 49′ 47.75″ W
D	46° 21′ 57.20″ N	98° 20′ 08.77″ W
E	20° 58′ 26.47″ S	55° 17′ 24.25″ E
F	43° 03′ 12.53″ S	65° 11′ 27.29″ W
G	10° 42′ 06.2″ N	61° 38′ 20.3′′ W
н	34° 36′ 53.26″ N	129° 27′ 12.49″ E

\*Mercury datum (1960)

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